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STS-3/OSS-1 PLASMA DIAGNOSTICS PACKAGE (PDP) MEASUREMENTS OF  
ORBITER TRANSMITTER AND SUBSYSTEM ELECTROMAGNETIC INTERFERENCE

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## 1.0 INTRODUCTION

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This report is intended to present a quick-look analysis of the Plasma Diagnostics Package (PDP) electromagnetic spectral measurements on the STS-3/OSS-1 mission from March 1982. Further interpretation of the data is awaiting ancillary information on the operation of Orbiter subsystems, such as thrusters and on the detailed trajectory and attitude.

The PDP receiver system is described to identify the various antennas and to characterize the complement of receivers which cover the frequency range of 30 Hz to 800 MHz and S-Band at  $2200 \pm 300$  MHz. Sample results are presented to show the variety of electromagnetic effects associated with the Orbiter and the time variability of these effects. The electric field and magnetic field maximum and minimum field strength spectra observed during the mission at the pallet location are plotted. Values are also derived for the maximum UHF transmitter and S-band transmitter field strengths. Finally, calibration data to convert from the survey plots to actual narrowband and broadband field strengths are listed.

Support for the PDP on the STS-3/OSS-1 Mission was provided through NASA/MSFC Contract NAS8-32807. OSS-1 Mission management was provided by NASA/GSFC.

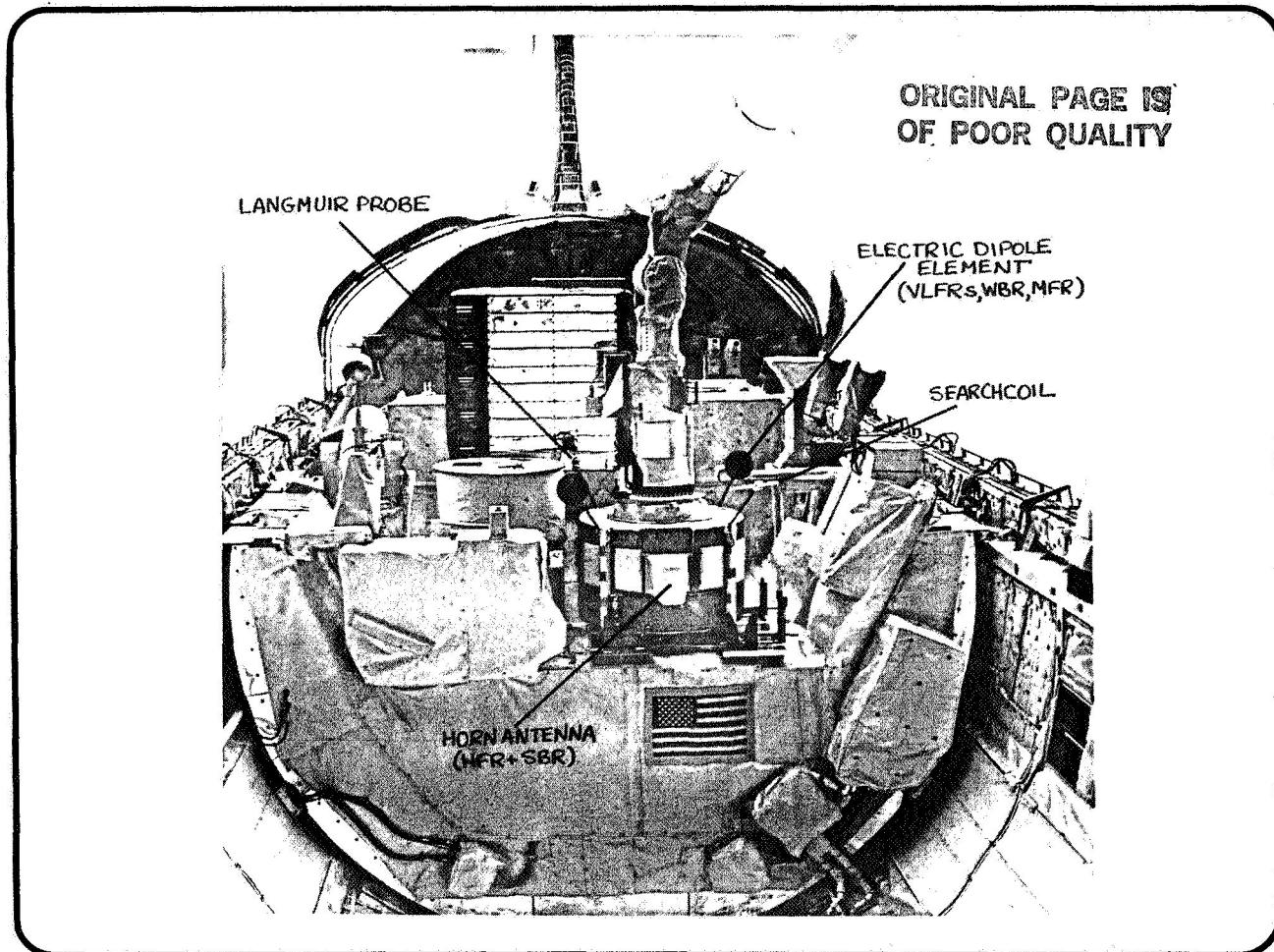
## 2.0 DESCRIPTION OF RECEIVER SYSTEM

Sensors for the detection of magnetic and electric wave fields are identified in Figure 1. Two spheres of 8 inch diameter, separated by 1.2 meters make up the electric dipole antenna which is utilized from DC to 20 MHz in frequency. Calibration measurements at NASA/GSFC before flight indicated that the effective electrical length of this dipole was only 0.22 meters because of the proximity to the PDP. For higher frequency electric fields, a broadband single polarization horn antenna is utilized. It covers the range of 20 MHz through S-band at 2200 MHz. In addition, the searchcoil sensor is used to detect the magnetic field component of electromagnetic waves from 30 Hz to 178 kHz. The Langmuir Probe is sensitive to electrostatic plasma waves over the same VLF range of 30 Hz to 178 kHz.

A block diagram of the PDP sensors and associated receivers is shown in Figure 2. One VLF range receiver from the IMP program VLFR-IMP is switched between the electric dipole, the searchcoil and the Langmuir Probe sensors every 51.2 seconds to provide 16 channels of VLF spectra--30 Hz to 178 kHz. In addition, the waveform is preserved in the Wideband Receiver (WBR) and this analog data is included in the PDP data stream. Every 12.8 seconds the WBR switches 10 kHz bands sequentially covering 0-10 kHz, 20-10 kHz and 20-30 kHz for each sensor. The VLFR-HELIOS always is connected to the electric dipole antenna to give a peak and average spectrum every 1.6 seconds.

The electric dipole also drives the Medium Frequency Receiver (MFR) which covers 316 kHz to 17.8 MHz in 8 channels. This MFR shares a logarithmic detector with the High Frequency Receiver (HFR) which has four broadband channels spanning the range of 20 MHz to 800 MHz. Bandwidths for the VLFR and MFR are narrower at  $\pm 15\%$  and  $\pm 30\%$ , respectively. By mixing the S-band signal down to the HFR frequency range, the same log detector is used for the SBR by time multiplexing. Both peak and average spectra are obtained each 1.6 seconds.

A summary of the receiver characteristics is given in Table 1. Detailed performance specifications for the receivers and the other PDP instrument are given in Table 2. Note that the stated field strength ranges are only approximate.



PDP on Pallet: Antennas Identified

Figure 1

Figure 2

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## PDP WAVE INSTRUMENTATION

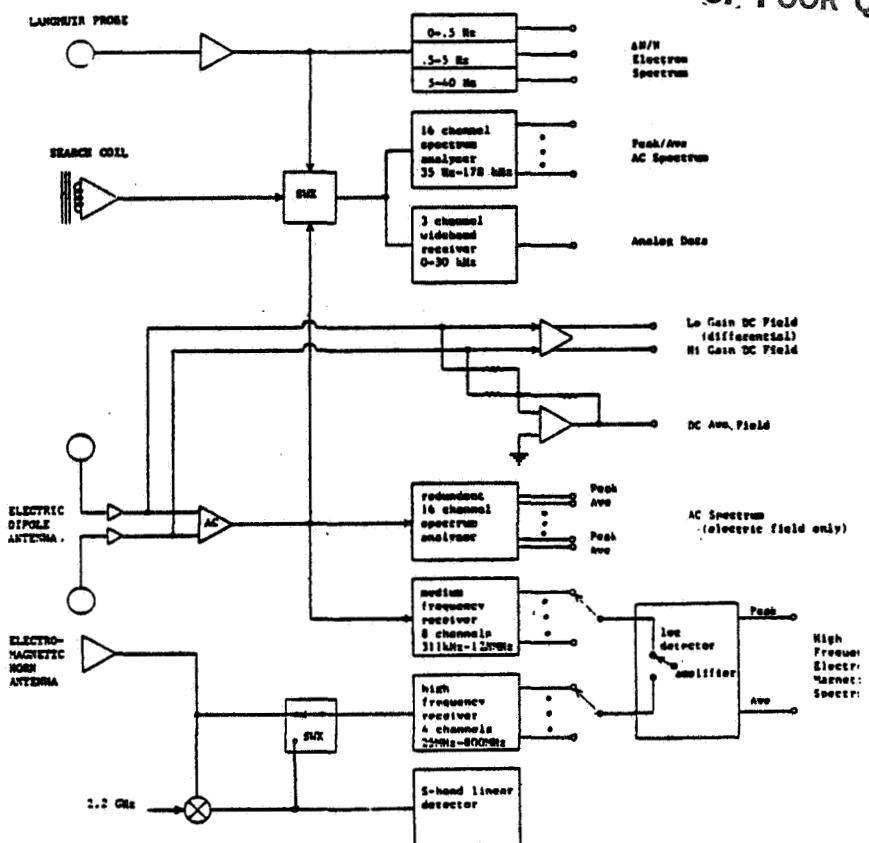


Table 1

## STS-3/PDP RECEIVER CHARACTERISTICS

VERY LOW FREQUENCY (VLFR)

- 16 CHANNELS
- 30 Hz TO 178 kHz

MEDIUM FREQUENCY RECEIVER (MFR)

- 8 CHANNELS
- 311 kHz TO 17.8 MHz
- 65 dB DYNAMIC RANGE

HIGH FREQUENCY RECEIVER (HFR)

- 4 CHANNELS
- 20 MHz TO 800 MHz

S-BAND RECEIVER (SBR)

- 4 CHANNELS WITH LOG DETECTOR
- 1 CHANNEL WITH LINEAR DETECTOR
- ~ 2200 MHz ± 300 MHz

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Table 2

PDP SCIENTIFIC INSTRUMENTS PERFORMANCE SPECIFICATIONS

| MEASUREMENT                         | TECHNIQUE   | PARAMETERS  | VALUE/RANGE   |
|-------------------------------------|---|---|---|
| DC Magnetic Field                   | Triaxial Fluxgate Magnetometer                                      | Dynamic Range<br>Temporal Resolution  | $\pm 12$ milligauss to $\pm 1.5$ gauss<br>each axis<br>10 samples/second each axis  |
| DC Electric Field                   | Im Double Probe with Spherical Sensors                              | Dynamic Range<br>Temporal Resolution  | $\pm 2$ mV/m to $\pm 2$ V/m (average and differential)<br>20 samples/second   |
| AC Magnetic Waves                   | Searchcoil Sensor; Wideband Receiver                                | Frequency Range<br>Amplitude Range<br>Duty Cycle  | 5Hz-1kHz & 0.65-10, 10-20,<br>20-30kHz<br>100db @ 0.4db resolution;<br>3mV-300V<br>12.8 seconds out of 51.2 sec.  |
|                                     | Searchcoil Sensor; VLF Spectrum Analyzer (IMP) VLFR-IMP             | Frequency Range<br>Frequency Resolution<br>Amplitude Resolution<br>Temporal Resolution<br>Duty Cycle    | 16 channels 35.5 Hz to 178kHz<br>$\pm 15\%$ bandwidth<br>100db @ 0.4dB resolution;<br>$3 \times 10^{-5}$ - $3 \times 10^{-1}$ V $\cdot$ Hz $^{-1/2}$<br>(peak and average)<br>0.6 sample/second each channel<br>12.8 seconds out of 51.2 sec. |
| AC Electric and Electrostatic Waves | Im Dipole Antenna Wideband Receiver WBR                             | Frequency Range<br>Amplitude Range<br>Duty Cycle  | 5Hz-1kHz, 0.65-10kHz, 10-20kHz<br>& 20-30kHz<br>100db @ 0.4db resolution;<br>3μV/m - 300 mV/m<br>38.4 seconds out of 51.2 sec.  |
|                                     | Im Dipole Antenna VLF Spectrum Analyzer (Helios) VLFR-HELIOS        | Frequency Range<br>Frequency Resolution<br>Amplitude Resolution<br>Temporal Resolution<br>Duty Cycle    | 16 channels-31.2Hz to 178kHz<br>$\pm 15\%$ bandwidth<br>100db @ 0.4dB resolution;<br>$3 \times 10^{-8}$ - $3 \times 10^{-3}$ V $\cdot$ Hz $^{-1/2}$<br>(peak and average)<br>0.6 sample/second each channel<br>100Z                           |
|                                     | Im Dipole Antenna, Mid Frequency Receiver MFR                       | Frequency Range<br>Frequency Resolution<br>Amplitude Resolution<br>Temporal Resolution                  | 8 channels-31.6Hz to 17.8 MHz<br>$\pm 30\%$ bandwidth<br>70db @ 1dB resolution;<br>$3 \times 10^{-3}$ - 10 V/m (peak and average)<br>1.6 second/scan  |
| VHF/UHF EMI Levels                  | Horn Antenna VHF/UHF Receiver HFR                                   | Frequency Range<br>Frequency Resolution<br>Amplitude Resolution<br>Temporal Resolution                  | 4 channels—25-65, 65-160,<br>160-400, 400-800 MHz<br>$\pm 50\%$<br>70db @ 1db resolution; $10^{-2}$ -<br>30 V/m; (peak and average)<br>1.6 sec/scan   |
| S-Band Field Strength Monitor SBR   | Horn Antenna VHF/UHF Receiver + Mixer and L.O.                      | Frequency Range<br>Amplitude Range<br>Temporal Resolution   | 2000-2330 MHz<br>.01 to 30 V/m (peak & average)<br>1.6 sec.   |
| Suprathermal Particles              | Low Energy Proton & Electron Differential Energy Analyzer (LEPEDEA) | Energy Range<br>Energy Resolution<br>Field of View<br>Flux: Electrons<br>Protons<br>Temporal Resolution | 2eV-50keV in 42 steps;<br>electrons and ions<br>34Z<br>$6^\circ \times 162^\circ$ (7 detectors)<br>$30-1 \times 10^7$ , electrons/cm $^2$ sec<br>sr eV<br>$6-2 \times 10^8$ protons/cm $^2$ sec sr eV<br>1.6 sec for spectrum                 |
|                                     | Electrometer  | Flux Range<br>Temporal Resolution   | $10^9$ - $10^{14}$ elect cm $^{-2}$ sec $^{-1}$<br>10 samples/second  |
|                                     | Retarding Potential Analyzer/Differential Ion Flux Probe            | Density Range<br>Energy Range<br>Velocity Range<br>Temporal Resolution                                  | $2 \times 10^1$ - $1 \times 10^7$ ions cm $^{-3}$<br>0-16 eV<br>0-15km sec $^{-1}$<br>0.8 sec/scan; 51.2 sec/<br>analysis   |
| Thermal Electrons                   | Langmuir Probe, Density   | Dynamic Range<br>Temporal Resolution  | $10^3$ - $10^7$ electrons cm $^{-3}$<br>1 second sweep every 12.8 sec.  |
|                                     | Langmuir Probe, Density Irregularities                              | Scale Sizes<br>Dynamit Range  | 10 meters to 100 km<br>80db @ 5db resolution; $10^2$ -<br>$10^8$ cm $^{-3}$   |
| Thermal Ions                        | Ion Mass Spectrometer   | Dynamic Range<br>Mass Range<br>Temporal Resolution  | $20-2 \times 10^8$ ions cm $^{-3}$<br>1-64 AMU @ < 1% overlap<br>1.6 seconds for mass scan  |
| Ambient Pressure                    | Ionization Gauge  | Pressure Range  | $10^{-7}$ to $10^{-3}$ torr   |

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### 3.0 OVERVIEW OF ORBITER AC ELECTRIC FIELD ENVIRONMENT

In Figure 3 is presented a 30 minute summary plot of the PDP measured electric fields from 30 Hz to S-band for GMT DAY 85 20:30 to 21:00. Noted in the figure are the variety of phenomena which have been detected during the mission. Note that for each frequency, the vertical scale represents approximately 100 dB of dynamic range.

Very short bursts in the VLF range near 20:37 and 20:39 are assumed to be due to thruster firings. The changing VLF field strength from 20:30 to 20:37 has been identified as a broadband electrostatic noise which is Orbiter-attitude dependent--it peaks when the plasma is rammed into the payload bay (-Z axis parallel to velocity vector). Also very obvious in the VLF range is the increased intensity as the Fast Pulse Electron Generator (FPEG) emits a 50 ma beam of 1 keV electrons. As the PDP is moved in and near the beam by the RMS (Remote Manipulator System), the noise is seen in the channels of the MFR. Probably these emissions occur near the electron gyrofrequency ( $\sim 1$  MHz) and the plasma frequency (3-10 MHz).

These FPEG generated plasma waves do not extend up into the HFR range, typically. At 271 MHz (165-400 MHz channel of the HFR) is seen the UHF downlink transmitter. Since the PDP is being rotated and positioned at various points just above the payload bay, it sees different S-band field strength levels as indicated.

Some of these effects are depicted in more detail in the next section.

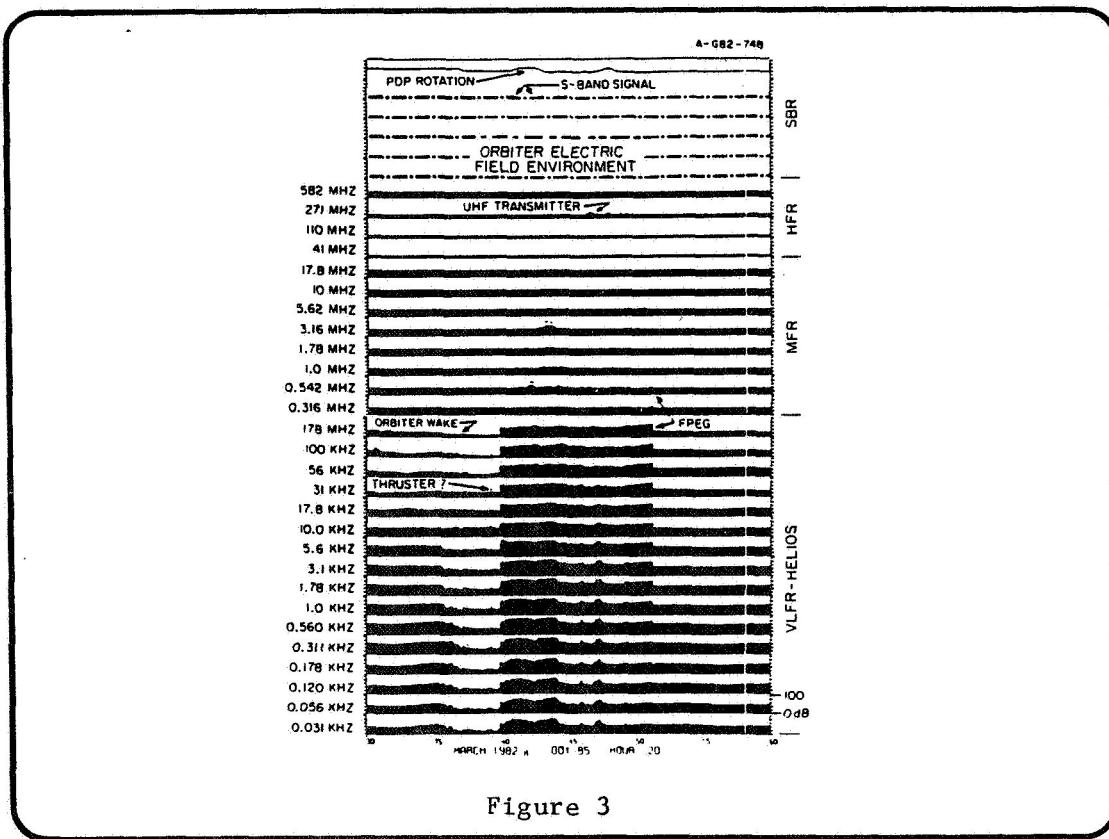


Figure 3

#### 4.0 TIME VARIABILITY OF OBSERVED NOISE

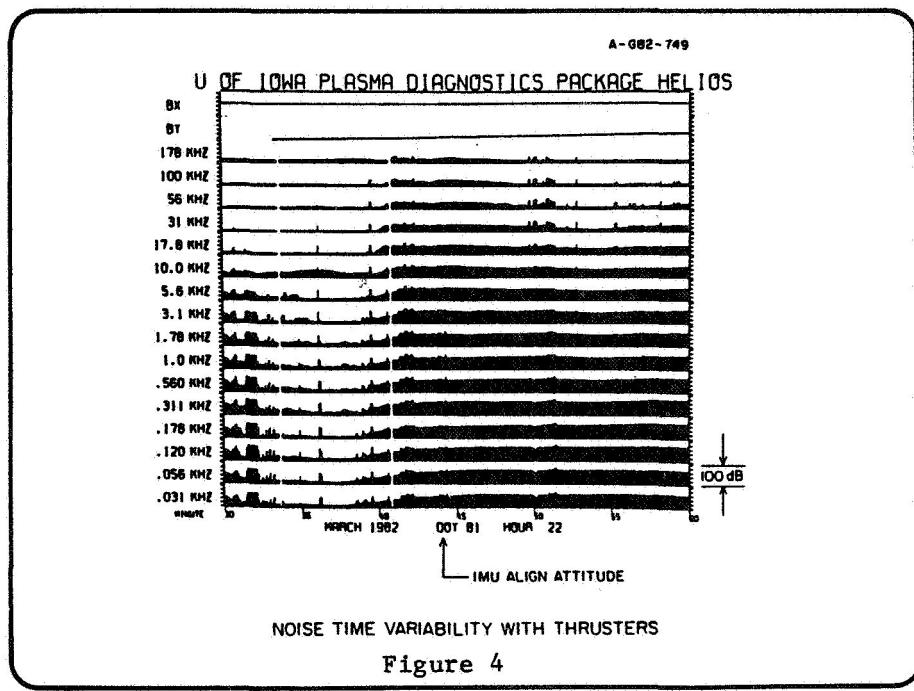
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The following series of figures illustrate the time variability of the VLF electric field noise from time scales of seconds to tens of minutes. Typically only the UHF and S-band transmitters are observed above 178 kHz because the receivers are less sensitive and plasma-related waves do not extend to frequency above 10 MHz. Thus waves at frequencies of a few hundred kilohertz to 20 MHz are not seen unless the FPEG is operating.

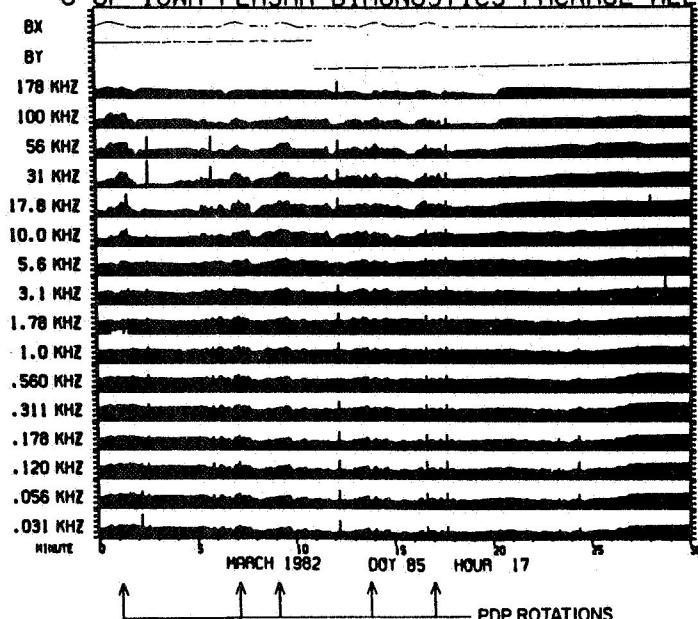
In Figure 4 is seen a ~ 60 dB overall amplitude change in the matter 10 minutes with short bursts of only seconds in duration. The overall trend is attributed to the Orbiter-attitude related electrostatic noise. Short bursts are most likely thrusters. For Figure 4, the PDP is stowed on the pallet whereas for Figure 5 the PDP is on the RMS. The overall levels are not much different but the levels do change with PDP rotation. This change indicates that the noise sources are either strongly polarized or what is more likely, localized on the Orbiter. Note that BX is a component of the earth's magnetic field which indicates the PDP rotation.

Experiment and Orbiter systems can definitely affect the signal strengths. When the FPEG operates, levels increase by ~ 20 dB. In the one case of a Primary Reaction Control System (PRCS) jet firing at GMT DAY 85 14:36, the noise actually decreases at the higher frequencies. The momentary gas output may moderate the Orbiter interaction with the plasma which produces the broadband electrostatic noise.

Evidence that the broadband electrostatic noise is not due to an Orbiter subsystem or instrument is presented in Figure 7 at the time of a payload bay door closing. During this three minute interval, the noise dropped below the receiver noise levels at all frequencies. Consequently, the noise does not originate inside the bay; it is shielded by the doors. When the doors are opened, the noise returns. If this noise is a significant problem to payload instrumentation, it can be minimized by directing the bay away from the velocity vector.



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SIGNAL STRENGTH VS PDP ROTATION

Figure 5

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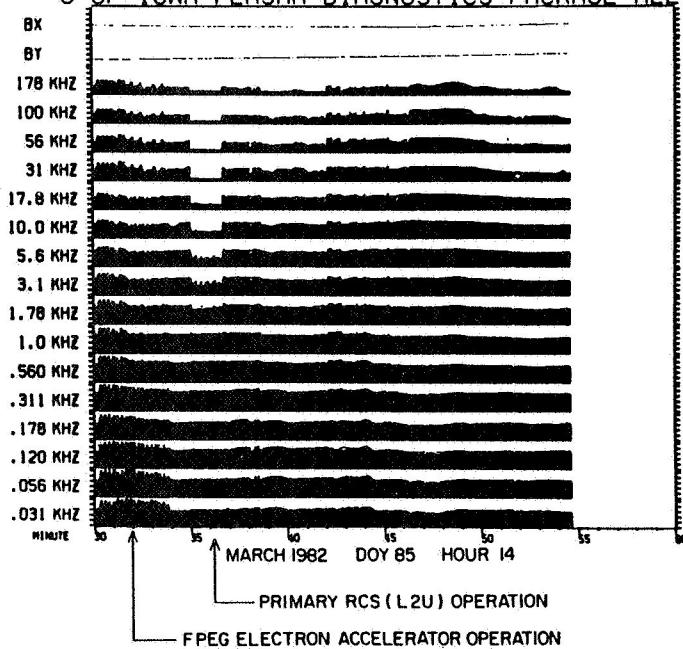
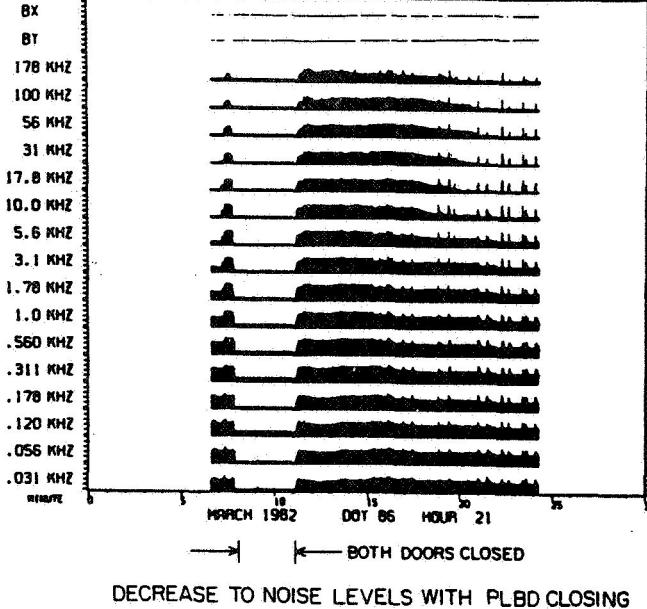


Figure 6

## U OF IOWA PLASMA DIAGNOSTICS PACKAGE HELIOS



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DECREASE TO NOISE LEVELS WITH PLBD CLOSING

Figure 7

## 5.0 SPECTRUM OF ELECTROMAGNETIC NOISE

Use has been made of the Wideband Analog Receiver (WBR) to determine the spectral nature of the electric field and magnetic field noise. Spectra covering 0 to 30 kHz for several minutes of time are shown in Figure 8. The magnetic field noise shows intense lines with spacings of Hz, kHz, 10's kHz, and harmonics. Further work is in progress to identify the exact frequencies and their change with time. It is surmized that these lines are associated with data clocks and power converters.

On the other hand, the electric field spectra show a "white noise" characteristic which does not change much with time. During the payload bay door closing, weak spectral lines were evident since the external broadband noise was screened out. Note that the WBR has an automatic gain control so that the amplitude variations of Figure 4, for example, are not evident.

By searching over extended periods while the PDP was stowed on the pallet, values for the minimum and the maximum noise levels have been obtained and displayed in Figure 9. These values are calibrated in volts per meter and normalized to a 1 MHz bandwidth. The electric scales as 20 log (electric field), whereas, the bandwidth scales as 10 log (bandwidth) as the data are presented. Also plotted for comparison are the broadband electric field limits for the Shuttle itself and for a payload. When the FPEG is not operating, above the 14 kHz cutoff, the maximum level (open circles) does not exceed the payload limit. When the FPEG operates with the PDP in the beam, the levels are increased by ~ 20 dB in the VLF range.

Narrowband magnetic field strengths are much less variable ( $< \pm 10$  dB) from the minimum to maximum observed levels. These levels are not Orbiter-attitude dependent and in fact, the levels were above the maximum door-opened levels with the payload bay doors closed. It is surmized that these levels are due to Orbiter subsystems which should be slightly time dependent as systems turn ON/OFF. During FPEG operations, levels in the 1-100 kHz range are increased.

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### DETAILED PDP NOISE SPECTRA

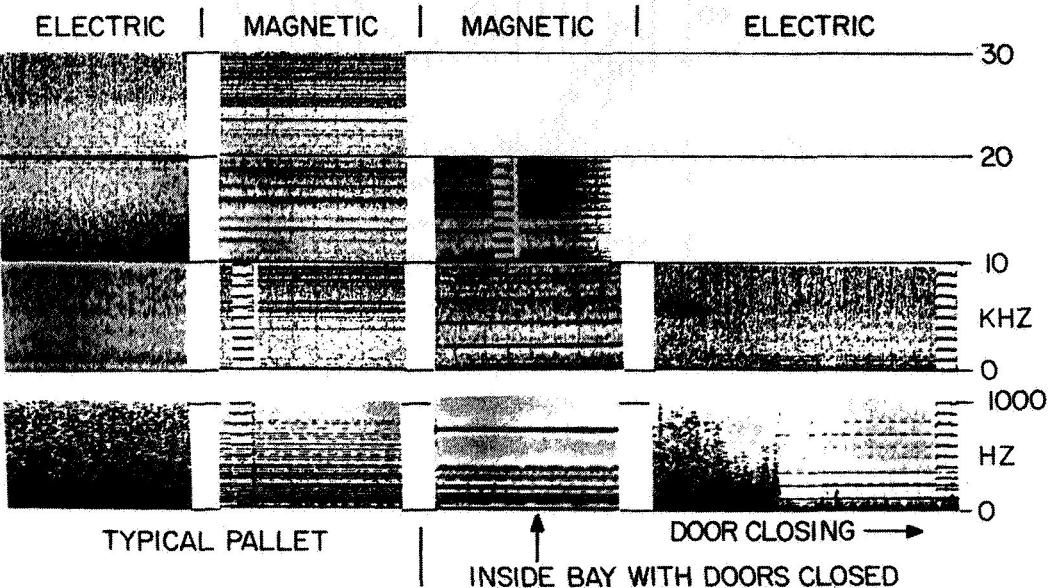


Figure 8

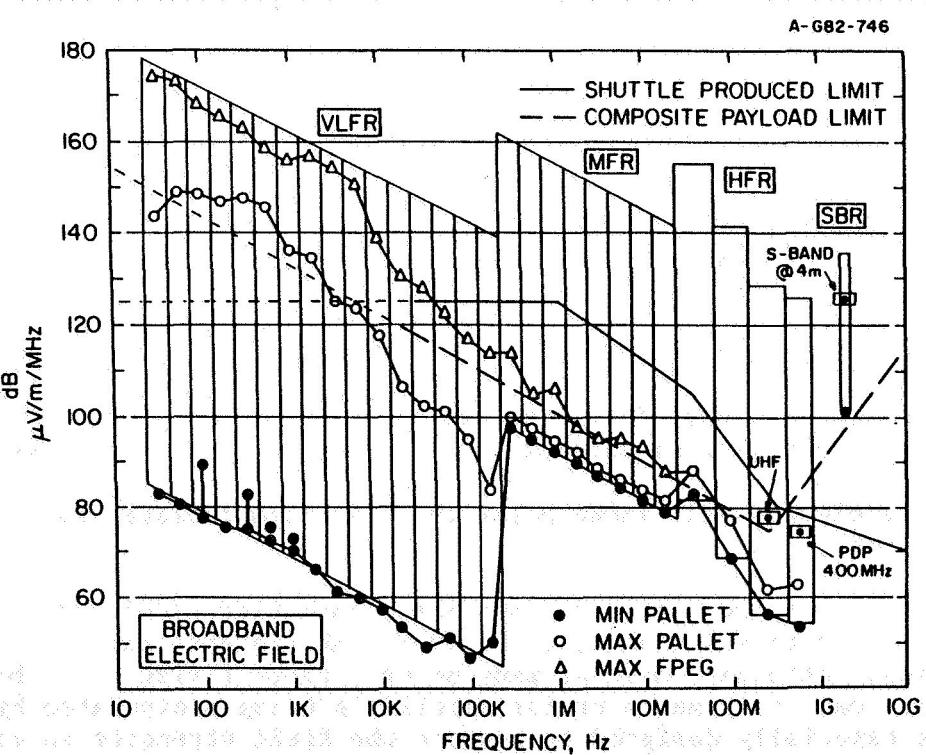


Figure 9

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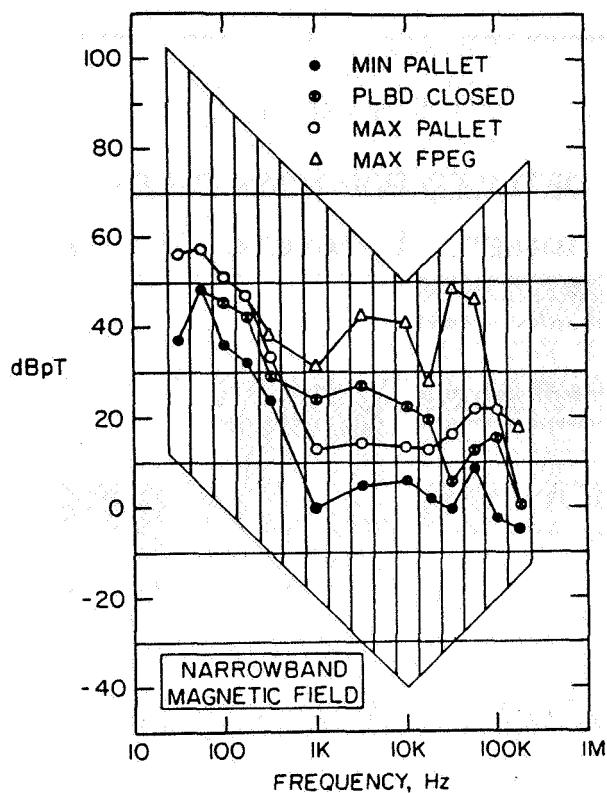


Figure 10

## 6.0 UHF AND S-BAND TRANSMITTER FIELD STRENGTHS

One filter channel of the PDP HFR covered the band of 165-400 MHz which includes the 295 MHz frequency of the UHF voice downlink transmitter. When this transmitter was keyed ON and connected to the upper antenna, a signal was detected by the PDP as shown in Figure 3. These measured field strengths were always below 0.5 V/m with the PDP on the RMS and below 0.1 V/m at the PDP pallet location. Average and peak field strengths are given in the following table:

| <u>Location/Field Strengths ± 2dB</u>   | <u>Average</u> | <u>Peak</u> |
|---|----------------|-------------|
| PDP on Pallet at 13 meters from Antenna | .05 V/m        | 0.08 V/m    |
| PDP on RMS at 8 meters from Antenna     | .23            | .44         |

These levels are well known below the suggested radiated susceptibility field strengths.

At S-band, the 150 watt data downlink transmitter (2287.5 MHz) can produce fields which are modeled to be 49.6 V/mR (meters) in the beam of the selected "quad" antenna. Even at many meters, these fields could be at damage level for payload instruments or for satellites being manipulated by the RMS. The SBR was especially designed to measure the field strengths in and around the payload bay as shown in Figure 3. These measured levels were about 5 dB ± 2 dB higher than the modeled values but comparable to a crude theoretically calculated value as follows:

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Field Strengths Relations  
(V/m)

|                                 |                  |
|---------------------------------|------------------|
| Predicted Field Strengths       | 49.6 /R (meters) |
| Measured with PDP ( $\pm 2$ dB) | 90.3 /R (meters) |
| Calculated @ (150 Watts)        | 94.9 /R (meters) |

The calculated value assumes that all of the power is emitted into a hemisphere ( $2\pi$  steradians) with 100% efficiency.

In the antenna beam, the fields exceed 20 V/m inside of 5 meters. However, with the PDP on the pallet at a range of 13 meters off the edge of the beam, the fields were not observed at the threshold of 2 V/m whereas the in-beam prediction would be 7V/m. Consequently, payload bay instrumentation is not subjected to damage levels.

#### 7.3 HFR

Because of the variety of bandwidths, the dynamic range is listed in the following table:

| <u>Center Frequency</u> | <u>Bandwidth</u> | <u>Minimum</u> | <u>Maximum</u> | <u>Slope</u> |
|-------------------------|------------------|----------------|----------------|--------------|
| 40 MHz                  | 20 - 65 MHz      | -40 dBV/m      | +32 dBV/m      | 16 dB/V      |
| 100                     | 65 - 165         | -40            | +32            | 16           |
| 250                     | 165 - 400        | -31            | +41            | 16           |
| 600                     | 400 - 800        | -22            | +52            | 16           |

$$\text{dBV/m} \sim \text{Maximum dB} + 16 \text{ dB V/m * Output Voltage -80 dB}$$

#### 7.4 SBR

Only the linear detector on the S-band system operated. An RF relay failure prevented the S-band signal from getting to the log-detector. Using calibrations at GSFC and Iowa before flight and re-calibration after flight, it is determined that the linear response is

$$\text{V/m} = 5.7 * \text{Output Voltage at } 2287.5 \text{ MHz Boresight}$$

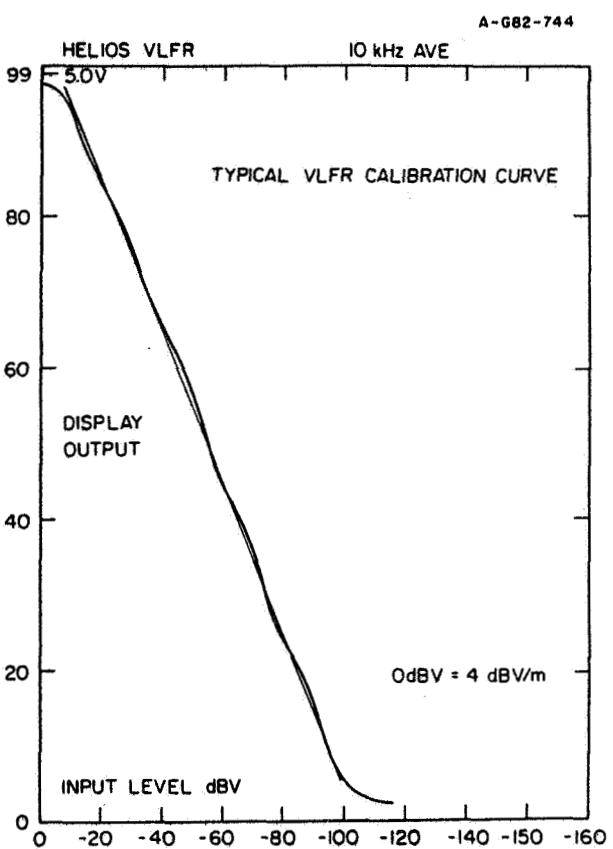
giving a fit to the field with range of about

$$\text{V/m} = \frac{90 \text{ V/m}}{\text{R (meters)}}$$

where R is the distance from the S-band quad antenna in the nominal beam.

#### 8.0 COMMENTS

Comprehensive sets of Orbiter noise spectrum measurements have been obtained. It is found that the noise levels do not exceed the worst case predictions for the Orbiter. Consequently, the receivers really need to be more sensitive to obtain the science and the EMI data on Spacelab-2 especially since the PDP measures the Orbiter at 100 meters range. It is hoped that these improvements in sensitivity can be made for Spacelab-2.



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Figure 11

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ADDITIONS TO  
DR. S. SHAWHAN  
PRESENTATION

TABLE 4

STS-3/PDP RECEIVER CHARACTERISTICS

VERY LOW FREQUENCY (VLFR)

- DOUBLE SPHERE ANTENNA FOR ELECTRIC FIELD
- SEARCH COIL ANTENNA FOR MAGNETIC FIELD
- 16 CHANNELS ( $\times 2$  SYSTEMS)
- 30 HZ TO 178 KHZ
- WIDEBAND RECEIVER 30 HZ TO 30 KHZ

MEDIUM FREQUENCY RECEIVER (MFR)

- 8 CHANNELS
- 311 KHZ TO 17.8 MHZ
- 65 DB DYNAMIC RANGE

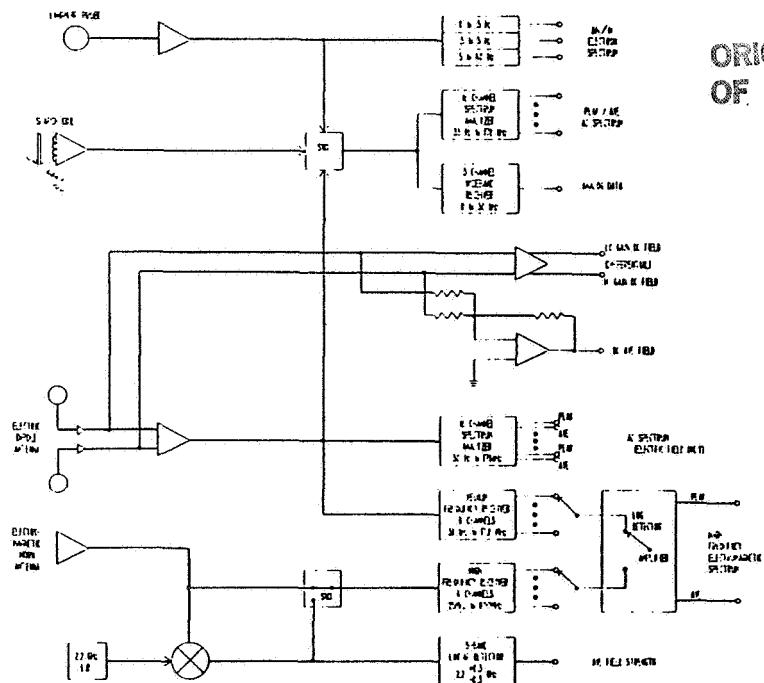
HIGH FREQUENCY RECEIVER (HFR)

- 4 CHANNELS
- 20 MHZ TO 800 MHZ

S-BAND RECEIVER (SBR)

- 4 CHANNELS WITH LOG DETECTOR (FAILED)
- 1 CHANNEL WITH LINEAR DETECTOR
- $\sim 2200$  MHZ  $\pm$  300 MHZ

PDP WAVE INSTRUMENTATION ON STS-3 / OSS-1



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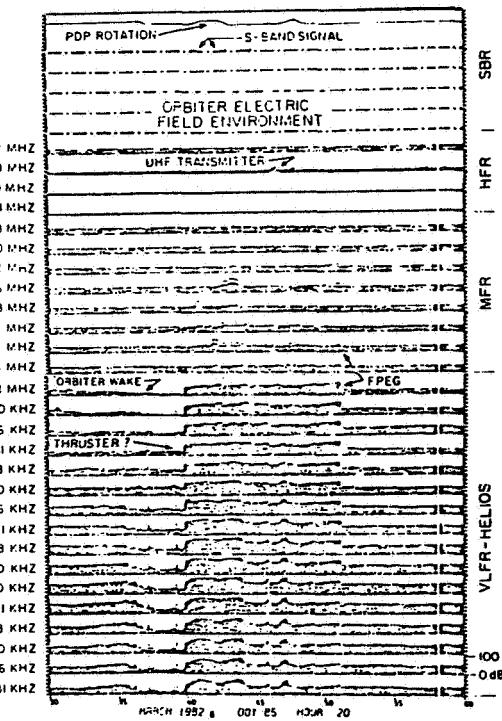


TABLE 17  
ORBITER-GENERATED ELECTROSTATIC NOISE

• OBSERVED CHARACTERISTICS

- Δ SPECTRAL EXTENT - 30 HZ TO 178 KHZ
- Δ SPECTRAL PEAK - 0.1 V/M @ 0.3 KHZ
- Δ VARIABILITY - 70 DB OVER ORBIT
- Δ MAGNETIC COMPONENT - NONE DETECTABLE OVER ORBITER MAGNETIC FIELD EMI
- Δ LOCATION - COMPLETELY DISAPPEARS WITH PAYLOAD BAY DOOR CLOSED;  
IMPLIES EXTERNAL TO ORBITER  
- NO SIGNIFICANT DIFFERENCE WITH PDP ON RMS; IMPLIES GENERATED  
IN LARGE VOLUME
- Δ THRUSTER RESPONSE - HIGH FREQUENCIES ( $> 10^4$  KHZ) ARE ATTENUATED  
DURING FIRINGS  
- LOW FREQUENCIES ENHANCED IF NOT ALREADY PRESENT
- Δ ORBITER ATTITUDE  
DEPENDENCE - MAX INTENSITY ~ RAM  
- MIN INTENSITY ~ WAKE  
- SEE LOW FREQUENCY AT ALL ATTITUDES EXCEPT EXACTLY WAKE  
- SEE HIGH FREQUENCY ONLY ~ RAM

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• TENTATIVE INTERPRETATION

- Δ WAVE MODE ION ACOUSTIC
- Δ PHASE/GROUP VELOCITY  $V \sim 2 \times 10^3$  M/SEC
- Δ MINIMUM WAVELENGTH  $\lambda_{(MIN)} \sim 2\pi a$  (DEBYE)  
 $\lambda_{(MIN)} \sim 0.02$  METERS
- Δ MAXIMUM DOPPLER SHIFT FREQUENCY  $F_{(MAX)} \sim V/\lambda_{(MIN)} \sim 100$  KHZ
- Δ MAXIMUM WAVELENGTH  $\lambda_{(MAX)} \sim 10$  LARMOR RADII
- Δ MINIMUM FREQUENCY  $F_{(MIN)} \sim V/\lambda_{(MAX)} \sim 30$  HZ

• POSSIBLE ORBIT ENERGY DISSIPATION

- Δ ENERGY DENSITY (STIX)  $W = \frac{\omega_i^2}{\omega^2} \cdot \left\{ \frac{1}{2} \cdot \epsilon_0 \cdot E^2 \right\}$  (MKS)
- $W \sim \left\{ \frac{50 \text{ kHz}}{300 \text{ Hz}} \right\}^2 \cdot \frac{1}{2} \cdot 9 \times 10^{-12} \cdot (0.1 \text{ V/M})^2$   
 $W \sim 1 \times 10^{-9}$  Joules/m<sup>3</sup>
- Δ VOLUME ESTIMATE  $V \sim (10 \text{ LARMOR RADII})^3 \sim (R_i)^3$   
 $V \sim 2.2 \times 10^5$  m<sup>3</sup>
- Δ TOTAL ENERGY/VOLUME  $W \cdot V \sim 3 \times 10^{-4}$  Joules
- Δ POWER  $P = \frac{W \cdot V}{10 R_i} \cdot \text{Velocity}$

$$P \sim 4 \times 10^{-2} \text{ WATTS}$$

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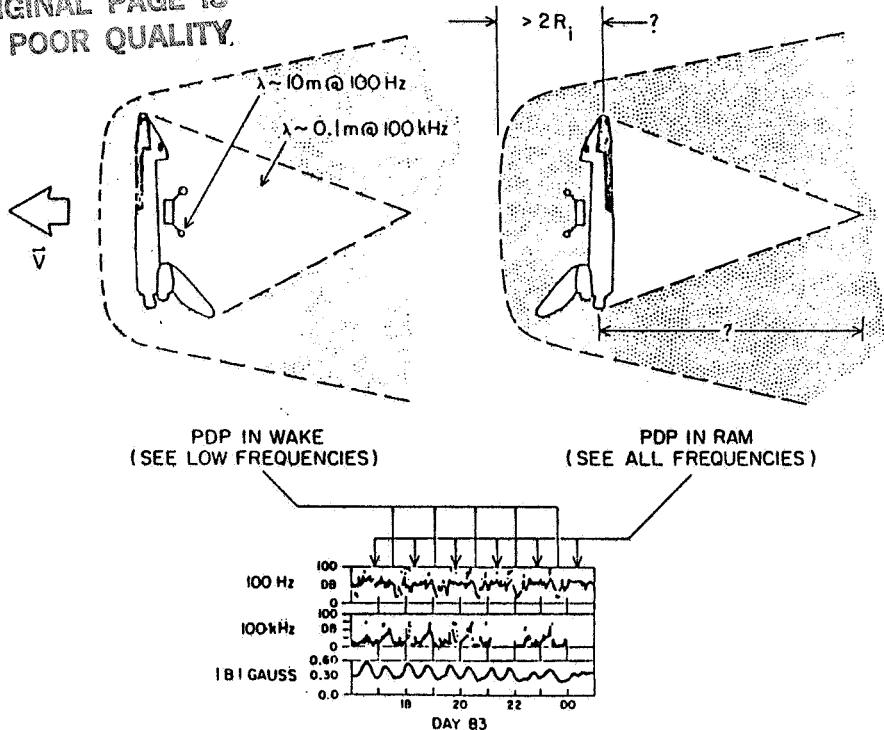


TABLE 9A

UHF/S-BAND TRANSMITTER FIELD STRENGTHS

UHF VOICE LINK (165-400 MHZ)

- Pallet Location: < 0.1 V/METER
- RMS SCANS: < 0.5 V/METER

S-BAND COMMUNICATIONS LINK (2200 ± 300 MHZ)

V/M @ 1M

|   |      |
|---|------|
| • MEASURED WITH PDP ( $\pm 2$ dB)             | 90.3 |
| • EXPECTED @ 150W                             | 49.6 |
| • CALCULATED @ 150W<br>(100% INTO HEMISPHERE) | 94.9 |